ARIZONA DEPARTMENT OF TRANSPORTATION REPORT NUMBER FHWA/AZ 82/175

FIELD AND LABORATORY EVALUATION OF SULFUR ASPHALT PATCHING MATERIALS

Prepared by: Frank R. McCullagh, P.E. Senior Research Engineer Arizona Transportation Research Center Arizona Department of Transportation

August, 1982

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Arizona Department of Transportation 206 South 17th Avenue Phoenix, Arizona 85007 in cooperation with The U.S. Department of Transportation Federal Highway Administration The contents of this report reflect the views of the authors who are responsible for the facts and the accuracy of the data presented herein. The contents do not necessarily reflect the official views or policies of the Arizona Department of Transportation or the Federal Highways Administration. This report does not constitute a standard, specification, or regulation. Trade or manufacturer's names which may appear herein are cited only because they are considered assential to the objectives of the report. The U. S. Government and the State of Arizona do not endorse products or manufacturers.

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INTRODUCTION

Patching deteriorated pavement is an important maintenance function. Proper patching extends the life of the pavement and improves the riding quality for the motoring public. A very expensive (labor intensive) and dangerous undertaking when under traffic, it is often not an effective procedure when improperly performed. Patches are frequently placed under adverse conditions (cold, damp, and in haste) and often not with the best materials; and because of this, they historically last only short periods of time.

There are three conventional patching techniques: 1) hot mixed, hot laid; 2) hot mixed, cold laid; and 3) cold mixed, cold laid. All of these are aggregate-asphalt mixtures with the last two containing some diluent in the asphalt. In Arizona, maintenance forces use cutback asphalt as the binder in their patching materials. These materials maintain their workability and do not have to be reheated during placement. Unfortunately, if placed under adverse weather conditions, distillates do not evaporate, the patch does not stabilize and is removed by traffic. To help with workability and compactibility, the gradation of the patch material is opened up to make it less dense. This allows water intrusion which further speeds up deterioration of the patch.

Another problem with the patching process is placement and compaction of material. Maintenance forces are usually attempting to maintain traffic around the work area and do not take the time to adequately prepare the pothole. Material is shoveled into the hole and a minimal amount of compaction applied. Ideally, the pothole should be cleaned out back to good dry material, tacked, and the patching material placed in layers and compacted.

Alternate binders may be required in the future because of environmental problems with cutbacks. One possible alternative is a composition of sulfur, asphalt, and sand (SAS) developed in Canada which consists of: 6% asphalt, 14% sulfur, and 80% sand. These are rough proportions though a normal mix will be in this range. It is self compacting, pourable, and very stable and the potential exists to place a durable patching material under adverse conditions.

The objective of this study was to develop a sulfur asphalt patching material and the procedures for placing them in the field, then to evaluate the performance of patches placed with SAS material.

LABORATORY EVALUATION

Several different sources of aggregate were investigated to develop a patching material. The goal was to use a source that would not need further processing which would reduce costs. Due to the high allowable voids in the mineral aggregate (VMA), it would also be possible to use aggregate sources that can not be used as is in asphalt concrete production. There are large supplies of blow sands in Arizona that could potentially be incorporated in a SAS mix. Two sources were tested and the mix design results are shown in Tables 1 and 2.

		<u>Table</u>	1. Pau	ilden Pi	t			
Sulfur %	12	12	12	12	14	14	15	15
Asphalt %	5	5	6	6	5	5	5.5	5.5
Marshall-Flow				8		10		9
Stability				1060		1331		988
Hveem Stability			28		23		27	
Voids	13.8	12.8	11.7	11.4	14.3	13.0	12.3	13.7
VMA	35.4	34.6	35.5	35.3	38.0	37.0	38.8	39.8
% Filled	61.0	63.0	67.0	67.6	63.4	64.9	71.5	62.7

	Table 2. Pi	t #5723		
Sulfur %	12	12	12	12
Asphalt %	5	5	6	6
Marshall Flow			9	
Stability			2310	
Hveem Stabili	ty			38
Voids	16.5	15.1	9.8	9.7
VMA	38.0	37.0	34.8	34.7
% Filled	56.6	59.2	71.8	72.0

The asphalt used was an AR2000 and the gradation of the aggregate is shown in Table 3 with Figure 1 being its grading curve.

Table 3. Aggregate Gradation (% Passing)

<u>Sieve Size</u>	<u>Paulden Pit</u>	<u>Pit #5723</u>
3/8	100	100
1/4	86	91
4	80	86
8	64	77
10	59	76
16	43	73
30	23	70
40	18	53
50	14	38
100	9	18
200	7	8

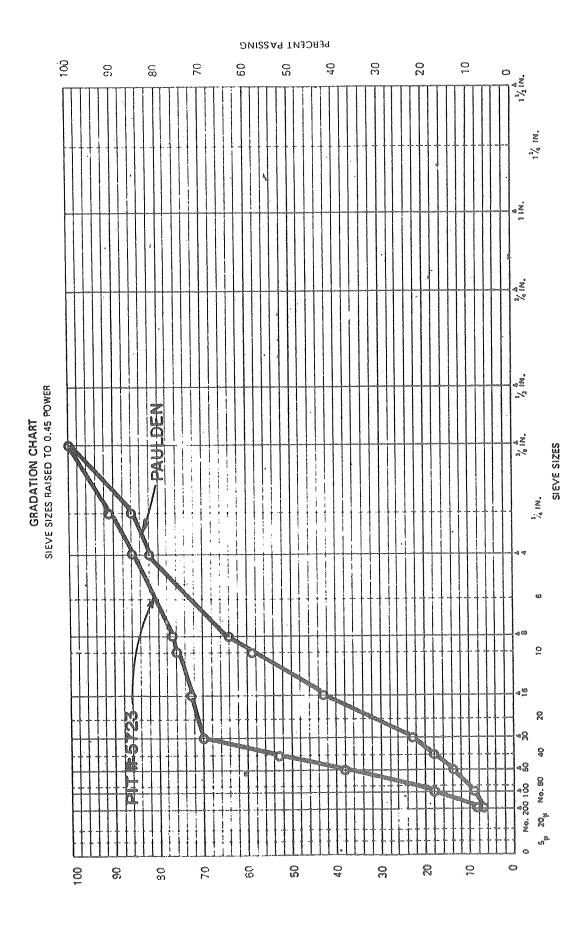


Figure 1. Aggregate Gradation

Specimens were not made in the normal manner. Materials were mixed at 275°F and poured into pre-heated compaction molds, rodded 25 times with a heated spatula and the top was troweled level. No other compaction was applied.

A problem associated with many Arizona aggregates and especially important with patching materials is that of water susceptibility. Specimens were prepared as above and tested by the Immersion-Compression test procedure. The specimens for both pits contained 6% asphalt, 12% sulfur, and 82% aggregate. The results are documented in Table 4.

Table 4. Immersion-Compression Results

	<u>Air psi</u>	<u>Water psi</u>	Retention %
Paulden Pit	148	76	51
Pit #5723	250	55	22

The results indicate Pit #5723 is highly water susceptible and for this reason, the Paulden Pit material was chosen for the field test.

FIELD EVALUATION

There were two objectives to this study. To develop a pourable, self-compacting and durable patching material and develop procedures to place this material in the field. From our work and that of others, it was apparent a material could be developed that might incorporate aggregate sources we are not presently able to use.

The second problem was more complicated. Sulfur asphalt sand must be placed at temperatures above 265°F, so a means of heating and keeping the material warm in the field was needed. A small asphalt recycling plant (Mini Cycle - Appendix A) was a potential solution. The plant is highly mobile, can heat the material to the required temperatures, and keep it warm. One major problem associated with all sulfur technology dealing with emissions did exist. In the plant, sulfur is exposed to direct flame if it is introduced during aggregate heat up. This would cause the evolution of sulfur dioxide (SO2) which could be hazardous if produced in sufficient quantities (greater than lOppm). Also hydrogen sulfide (H2S) would be produced if the temperature of the mix rose above 310°F. The following procedures were used in an attempt to avoid emission problems:

- 1. Clean the drum by running virgin aggregate through it and heating (approximately 300°F).
- 2. Place aggregate in drum.
- 3. Heat aggregate to 2750F.
- 4. Turn off the flame.
- 5. Add the sulfur and asphalt.
- 6. Mix and empty drum.
- 7. Repeat the cycle.

This procedure did not produce the desired results. The second cleaning of the drum, now with sulfur asphalt coating it, produced high SO2 emissions (greater than 50 ppm) all around the drum. Emissions of both SO2 and H2S were continuously monitored during this operation with an Interscan SO2 gauge and an Ecolyzer H2S gauge. During the rest of the production low levels of both gases were recorded and the SAS mix produced was thoroughly mixed and well coated. The problem though of SO2 production during clean out makes this approach unacceptable.

Several other approaches were considered but all required more equipment and personnel. The concept of SAS patching materials has potential but is being put aside until new equipment is developed.

RECYCLED PATCHING MATERIALS

As a part of this study, the Mini Cycle was initially used to patch pavements with recycled materials. This was done to familiarize the crew with the operation of the equipment and determine if any modifications needed to be made. When it was found the Mini Cycle could not be used for sulfur asphalt patching, more work was done with it using recycled materials.

Results of the work in both ADOT's Districts 5 and 7 indicate a superior patch can be placed using the Mini Cycle and recycled materials. Work in District 5 was accomplished during the winter when normal patches are destroyed in several days, patches placed with the Mini Cycle were in excellent shape after two weeks in service. The operation in District 7 was more successful. They experimented with several materials, temperatures and varied the operation of the equipment. Results indicate these patches will not need any repair.

There are several reasons for success with recycled patches. First, material was hot when placed and care was taken to compact it and properly prepare the pothole before patching. The size of the crew used and the equipment was thought to be an economic problem by District 5 though District 7 showed the hot recycled patching operation to be less expensive. When longevity of the patches is taken into account with the reduced danger to the crew and improvement due to less traffic disruption; this appears to be a better procedure. More information on the actual operation appears in reference 14.

CONCLUSIONS

- 1. Pourable, self-compacting sulfur asphalt mixtures can be developed using marginal aggregate sources.
- 2. The Mini Cycle can not be used to make sulfur asphalt patches alone without producing unacceptable levels of SO₂ emissions.
- 3. Recycled materials can be used to produce superior patches with the Mini Cycle.

APPENDIX

General Specifications - Mini Cycle Plant

Mixing and Heating Chamber

- 36" diameter x 48" long with 17" cone Size

Capacity - 3 to 8 t.p.h.

Construction - electrically welded all steel

Drum & Cone - 3/16m steel

Insulation - R 113-3 1/2" fiberglass compressed to 1"

Skin - .051 aluminum

8 flites 3/4" angle iron tangently placed61 1/2" x 3" studs Mixer

Tumbler

- 17" combination lump feed, heat inlet, and exhaust Port

port

Feed (Sized Material)

Hopper - 3 cubic feet

- 8" screw feeder 2 to 8 t.p.h. Feed

Burner

Fuel - 750,000 BTU, propane

- 6" naturally aspirated 2" venturi Size

Drive

Gas engine with manual clutch

6:1 gear reducer with V-belt drive

H.D. machined pulleys "B" Section 2 groove with counter shaft

H.D. sprockets with No. 80 chain drive

4 heavy-duty roller bearing trunnions

Frame and Towing Tongue

Electrically welded 2x3x1/8 and 3x3x1/8 box tubing

Wheels and Suspension

15" wheels - with 4 ply rated pneumatic tires

Fenders - 14 ga. steel

-2x2-3/16 box tubing Axle Springs - 1400 lbs. spring leaf

Engine House

14 ga. steel with engine throttle, off/on switch and clutch control

Towing Empty Weight

Axle - 1150 lbs. - 200 lbs. Frame Total $-\overline{1350}$ lbs.

Dimensions

Overall width - 56"
Overall height - 63"
Overall length - 143"

Power Unit

Model EY27W Wisconsin Robin Engine air cooled, 7 1/2 HP single cylinder 4 cycle 16.26 cubic inch, H.D. cast iron liner, forged steel crank shaft, ball main bearings both ends, bore 2.91" stroke 2.44", 1.45 gallon fuel tank, 1.6 pint oil capacity. This power is subject to availability and may be substituted.

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